GeoClaw and Tsunami Modeling: unique numerical aspects and future directions

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Numerical methods and software development:

- Randall LeVeque, University of Washington.
- Marsha Berger, Courant Institute, NYU.
- Kyle Mandli, University of Texas, Austin.
- Donna Calhoun, Boise State University.
- David Ketcheson, KAUST.
- Dave Yuen, University of Minnesota.

Geophysical modeling:

- Richard Iverson, U.S. Geological Survey.
- Roger Denlinger, U.S. Geological Survey.

• Survey of some unique numerical issues for tsunami modeling

- well-balancing for ocean propagation
- depth-positivity (wet/dry problem)
- shoreline instabilities
- ill-posedness and instabilities (e.g., resonance, roll waves, etc.)
- Introduction to granular-fluid flows
 - modeling multiphase "non-rheological" flows
 - coupling with tsunamis?

- well-balancing has to do with numerically maintaining particular steady-states
- required to resolve small perturbations to those steady-states
- cannot be determined by order of accuracy or convergence \rightarrow should be satisfied on coarse grids











Flow dynamics are small perturbations to a balanced steady state:

$$\begin{aligned} q_t + \mathcal{A}(q) q_x &= \psi(q, x, y), \\ \mathcal{A}(q) q_x &\approx \psi(q, x, y) \end{aligned}$$



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- applications with delicate balanced steady states require specialized methods.
- a numerical scheme is well-balanced if it exactly preserves discontinuous steady-state weak solutions.
- traditional schemes do not satisfy this property.



Balance law $q_t + f(q)_x = \psi(q, x)$

• Steady states arise when $f(q)_x = \psi(q, x)$



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- step 2: $Q^* \to Q^{n+1}$: solve ODEs for the source term: $q_t = \psi(q,x)$



• Preserving steady states $q_t + f(q)_x = \psi(q, x)$.

•
$$\mathcal{W} = [q, \varphi(q), b]^T$$
: $\mathcal{W}_t + \mathcal{A}(\mathcal{W})\mathcal{W}_x = 0.$

• The steady state field

$$\mathcal{A}(\mathcal{W})\mathcal{W}_x = 0, \quad \Rightarrow \mathcal{W}_x = r^0(\mathcal{W}), \quad \lambda^0(\mathcal{W}) = 0$$



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- motionless steady states: stationary steady state wave only



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Balance law $q_t + f(q)_x = \psi(q, x)$: steady state wave

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- shallow water equations present difficulties where $h \rightarrow 0$
- determining the motion of the shoreline can be difficult
- often ad hoc approaches are used
- this is prone to numerical instabilities

$$\begin{split} \frac{\partial h}{\partial t} + \frac{\partial (hu)}{\partial x} &= 0,\\ \frac{\partial (hu)}{\partial t} + \frac{\partial}{\partial x} (hu^2 + \frac{1}{2}gh^2) &= -gh\frac{\partial b}{\partial x}, \end{split}$$

- the equations are only valid where h>0
- the Riemann problem between wet and dry states can be exactly solved
- \rightarrow only for the homogeneous problem (no bathymetry!)

$$\frac{\partial h}{\partial t} + \frac{\partial (hu)}{\partial x} = 0,$$
$$\frac{\partial (hu)}{\partial t} + \frac{\partial}{\partial x} (hu^2 + \frac{1}{2}gh^2) = -gh\frac{\partial b}{\partial x},$$

motionless steady state at the shoreline: no waves.







































Overland flooding: Malpasset dam, France 1959



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Landslides and Debris Flows

Debris flows, landslides etc.: liquified masses of soil and rock.



Indonesian Lahar Movie Ritigraben Switzerland Debris Flow Movie

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Mobilization: $q_t + f(q)_x + \mathcal{W}(q)q_x = \psi(q, x)$

- failure occurs when the driving forces slightly exceed the shear strength at any one point: a small perturbation to a balanced steady state: $f(q)_x + \mathcal{W}(q)q_x \approx \psi(q,x)$
- failure: an equilibrium is perturbed...what happens next?

 - **2** quick stabilization: (shear dilation \rightarrow decreased pore pressure \rightarrow shear strength reestablished \rightarrow localized slump.)
 - **3** anything intermediate...*e.g.*, stick-slip.
- modeling the outcome at least requires well-balanced methods...if it can be done at all. Numerical conservation must be maintained for $f(q)_x$ while simultaneously being well-balanced.

Model equations are depth-averaged:



- Integrating out the vertical component gives 2D system for h, u, v, m, p_b
- degree of accuracy lost upon depth-averaging depends on shallowness;
- computationally tractable for large-scale problems.

Model equations are a hyperbolic system:



- similar in form to the shallow water equations;
- strictly hyperbolic system (desirable stability properties);

$$\begin{aligned} q_t + \mathcal{A}(q) q_x + \mathcal{B}(q) q_y &= \psi(q), \\ \text{where} \quad q = (h, hu, hv, hm, p_b)^{\mathrm{T}} \end{aligned}$$

• coupled evolution of pore pressure and solid-volume fraction

Pore-fluid pressure solid-volume fraction coupling:



- dilation/contraction of solid phase affects pore-pressure
- pore-pressure mediates Coulomb solid stress through buoyancy (effective stress)
- frictional stress determines stability of sediment mass
- dilation/contraction based on dilatancy angle
- feedback loop: shearing ⇔ contraction/dilation ⇔ pore-pressure ⇔ frictional resistance

Modeling mobilization/stability:



- an initial rise in pore pressure can perturb stability
- evolution and feedback determine whether mass destabilizes into debris flow
- contractive case: shearing leads to higher pressure & less resistance (positive feedback)
- dilative case: shearing leads to lower pressure & higher resistance (negative feedback)



Play Movie

Simulating natural initiation by rising pore-pressure

Simulating natural initiation by rising pore-pressure

Comparison of fluid-pore pressure



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Play Movie
USGS experimental debris-flow flume

Comparison of downstream (32m) depth and fluid-pore pressure



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- depth-averaged models can be coupled
 - landslide \rightarrow tsunamis through "dtopo"
 - landslides \leftrightarrow tsunami
 - granular-fluid model near inundation fronts
- always consider the possibility of numerical artifacts and/or instabilities in numerical solutions.
- validate, verify, compare, share.

Thank You!